# The contact of elastic regular wavy surfaces revisited

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## Roughness

- Roughness topologies play important role in contact mechanics (friction, adhesion, etc...)
- Self-affinity is often used to describe roughness
- The simplest possible 3D roughness is bi-sinusoidal







Stanley and Kato

### Variational approach

$$\begin{array}{ll} \textit{min} \quad f = \frac{1}{2} \int_{S} pu(p) dS + \int_{S} pg(p) dS \\ \\ p \geq 0 \qquad \frac{1}{A_0} \int_{S} p dS = p_0 \end{array}$$

#### SQP approach

 $\nabla f = u + g$ 

Enforce  $\int_{S} p dS = A_0 p_0$  by dichotomy

Fourier space computation of influcence functions Convergence depends on #points



double sin wave

#### Problem settings

- Isotropic material E\*
- small deformations
- Frictionless, non-adhesive contact
- Discretization 4096<sup>2</sup> points
- Periodic boundary conditions
- 200 load steps
- until full contact

Johnson, Greewood, Higginson. Int.J.Mech.Sci. 27, 1985. Krithivasan, Jackson. Tribol.Lett. 27, 2007



 $\mathsf{z}(x,y) = Bcos(2\pi x/\lambda)cos(2\pi y/\lambda)$ 

### @ infinitesimal contact

Hertz theory

• Curvature is 
$$R = 4\pi^2 B/\lambda^2$$

$$A' = \pi \left(\frac{3p_0}{8\pi p^\star}\right)^3$$

#### Near full contact

Pressurized crack assumption (Greenwood, IJSS, 56, 2015)  $A' = 1 - \frac{3}{2\pi} (1 - p')$ 



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$$n = \pi \left( 8\pi p^{\star} \right)$$

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## Contact area evolution

#### Comparison with simulation results

### Convexity change

- Contact area variation has 2 inflexion points
- Related to two (unexpected) extrema of the mean pressure

#### Overlooked

- Numerical restrictions did not provide intermediate points
- Why is mean pressure droping?



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- Becomes square-like : Loss of convexity
- Merging of contact zones
- Contact area grows more rapidly that pressure



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## Contact perimeter

Compactness of contact area

#### Perimeter evaluation

S = # contact transitions



## Compactness evaluation

$$\mathcal{C} = rac{S}{\sqrt{A}}$$
  
 $\mathcal{C}_{circle} = 2\sqrt{\pi}$   
 $\mathcal{C}_{square} = 4$ 

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#### Compactness evaluation

$$\mathcal{C} = rac{S}{\sqrt{A}}$$
  
 $\mathcal{C}_{circle} = 2\sqrt{\pi}$   
 $\mathcal{C}_{square} = 4$ 

#### Properties of the perimeter

- Wrong if curved
- Exact if square

## Correction of the perimeter

$$S = rac{S^d}{\eta(A')n}$$

- $S^d$  the "discrete" perimeter
- η(A') interpolates from circle to square compactnesses



## Contact perimeter

#### Compactness of contact area



$$p(x, a) = 2p_0 \frac{\cos(\frac{\pi x}{\lambda})}{\sin^2(\frac{\pi a}{\lambda})} \sqrt{\sin^2(\frac{\pi a}{\lambda}) - \sin^2(\frac{\pi x}{\lambda})}$$





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### Simulation pressure profiles

- Fits the assymptotic values
- Junction cancels the pressure profile slope


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#### PDF of pressures

$$P( ilde{
ho}) = rac{1}{A_0} \int_{A_0} \delta( ilde{
ho} - p(x,y)) dx dy$$

Property

$$\int_{ ilde{
ho}} P( ilde{
ho}) d ilde{
ho} = A_0/A_0 = 1$$

#### Numerical measure

- Decomposition in bins
- Intractable PDF function at the limit to zero



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#### Hertz analytic solution at small contact

Hertz:

$$P(\tilde{p},p_0)=\frac{8}{9}\tilde{p}$$

Full contact:

$$egin{aligned} \mathcal{P}( ilde{
ho}) &= rac{4}{\pi} rac{F(rccos( ilde{
ho}-1),1/\sqrt{2 ilde{
ho}- ilde{
ho}^2})}{\sqrt{2 ilde{
ho}- ilde{
ho}^2}} \ with \quad F(l,k) &= \int_0^l 1/\sqrt{1-k^2sin(x)}dx \end{aligned}$$



Evolution with load



Evolution with load



#### Persson's model (elastic case)

- Manipulate the Probability density function  $P(p, \zeta)$
- $\blacktriangleright$  as a Function of the applied pressure p and magnification  $\zeta$
- Under full contact assumptions we obtain

$$rac{\partial P(\pmb{p},\zeta)}{\partial V} = rac{1}{2} rac{\partial^2 P(\pmb{p},\zeta)}{\partial^2 \pmb{p}}$$

- ▶ where *V* is the variance of the pressure distribution.
- V is approximated by Persson as the variance achieved at full contact (elastic correlation to the heights profile):

$$V = \frac{1}{2} E^{\star} m_2(\zeta) = \frac{\pi E^{\star}}{2} \int_{k_1}^{\zeta k_1} k^3 \Phi^p(k) dk$$

Greenwood and Manners. Some observations on Persson's diffusion theory of elastic contact. Wear 261, 2006

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Persson's assumptions

#### Persson's assumptions

- ▶ In the derivation of the diffusion equation: full contact is assumed
- Need for a boundary condition to precise solution:

 $P(p=0,\zeta)=0$ 



Persson's assumptions

# How is the wavy surface result supposed to impact Persson's assumption ?



Persson's assumptions

#### Splitting the contact spots

$$P( ilde{
ho}) = rac{1}{A_0} \int_{A_0} \delta( ilde{
ho} - 
ho(x,y)) dxdy$$





Persson's assumptions

#### Splitting the contact spots

$$P(\tilde{p}) = \frac{1}{A_0} \int_A \delta(\tilde{p} - p(x, y)) dx dy + \frac{A_0 - A}{A_0} \delta(p)$$





Persson's assumptions

We are interested in the region  $0 < \tilde{p} < \epsilon$ :

$$\mathcal{P}( ilde{
ho}) = rac{1}{A_0}\sum_{i}^{m{N}(\epsilon)}\int_{A_i(\epsilon)}\delta( ilde{
ho}-m{p}(x,y))dxdy$$



Persson's assumptions

#### We want to investigate the limit when $\epsilon \rightarrow 0$ :

$$P( ilde{
ho}) 
ightarrow rac{1}{A_0} \sum_i^{N(0^+)} \Gamma(p_0')$$

where  $\Gamma(p'_0)$  is the pdf of patches of contact





Persson's assumptions

One should estimate the spatial density of asperity merging sites  $D(p_0')$  for which  $\Gamma(p_0')\neq 0$  :

$$P( ilde{
ho}=0+) = rac{1}{A_0}\sum_{i}^{D(
ho_0')A_0} \Gamma(
ho_0') \simeq D(
ho_0') \Gamma(
ho_0')$$

#### Missing ingredients

- $\Gamma(p'_0)$  the average PDF of pressure for merging asperities
- $\blacktriangleright$   $D(p_0')$  the spatial density of asperities merging at applied pressure  $p_0'$

Persson's assumptions

## Simulation Zoom (1/64)





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#### Overlooked particularity of bi-sinusoidal surface

- Area of contact: change of convexity
- Mean pressure: unexpected drop
- Perimeter: correction of numerical results is needed
- At full contact:  $P(0^+) \neq 0$

V.A. Yastrebov, G. Anciaux, J.F. Molinari, The contact of elastic regular wavy surfaces revisited. Tribol.Lett. 56, 2014

#### Future work

• Is it generalizable that  $P(0^+) \neq 0$ ?

